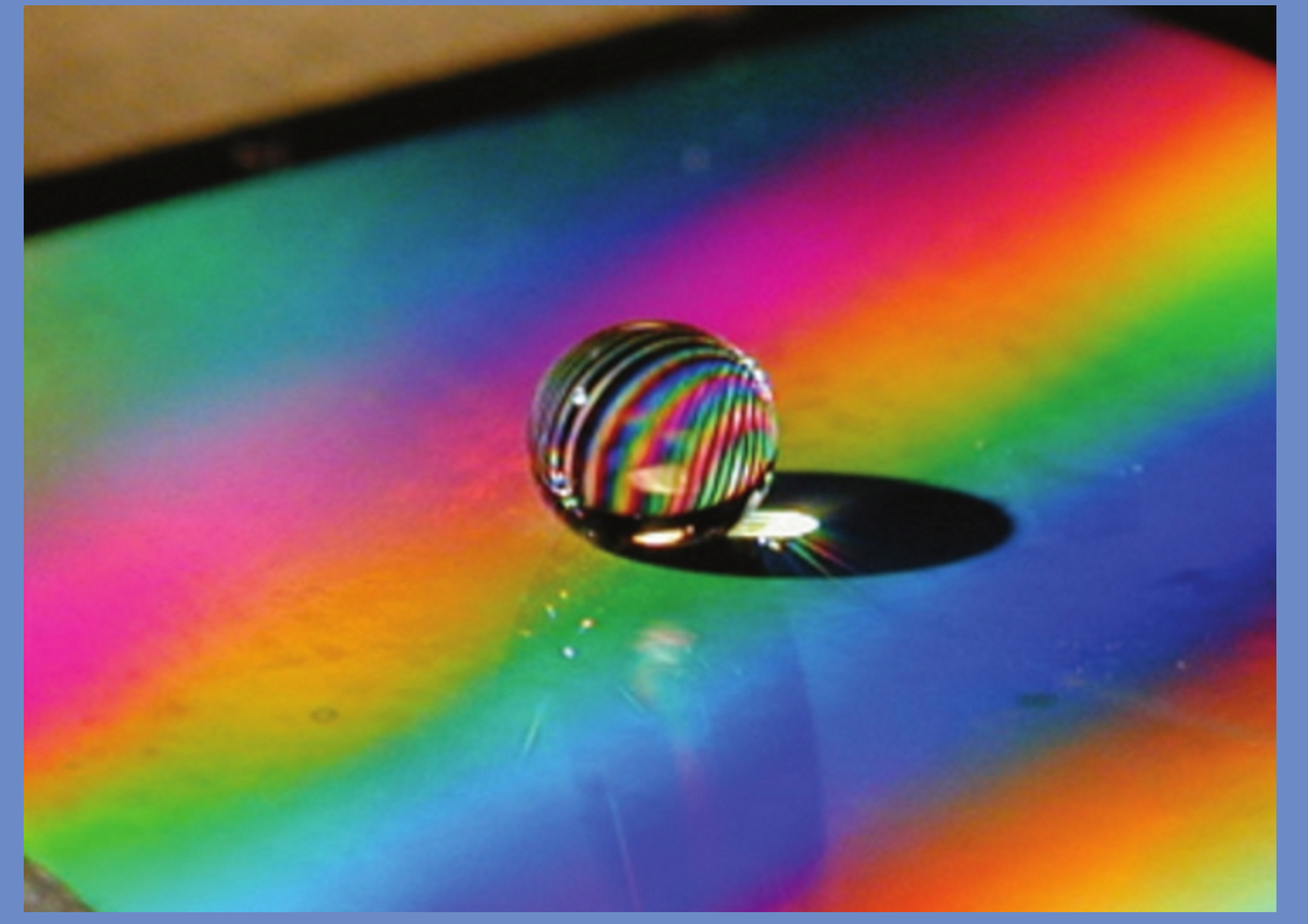


# A phase field approach to wetting and contact angle hysteresis

Antonio DeSimone and Livio Fedeli, SISSA - International School for Advanced Studies, Trieste, Italy



SCUOLA INTERNAZIONALE  
SUPERIORE di STUDI AVANZATI  
International School  
for Advanced Studies  
via Beirut 2-4 • 34014 Trieste • ITALY  
T +39 040 3787 11 • F +39 040 3787 528  
www.sissa.it



## 1. Physical review

Liquid drops can adhere to vertical or inclined plates by exploiting surface tension and frictional forces that can pin the contact line. These forces give rise to a phenomenon, called **contact angle hysteresis**, that allows the drop to adapt its contact angles and resist to gravity. In a two dimensional geometry the drop is in equilibrium if:

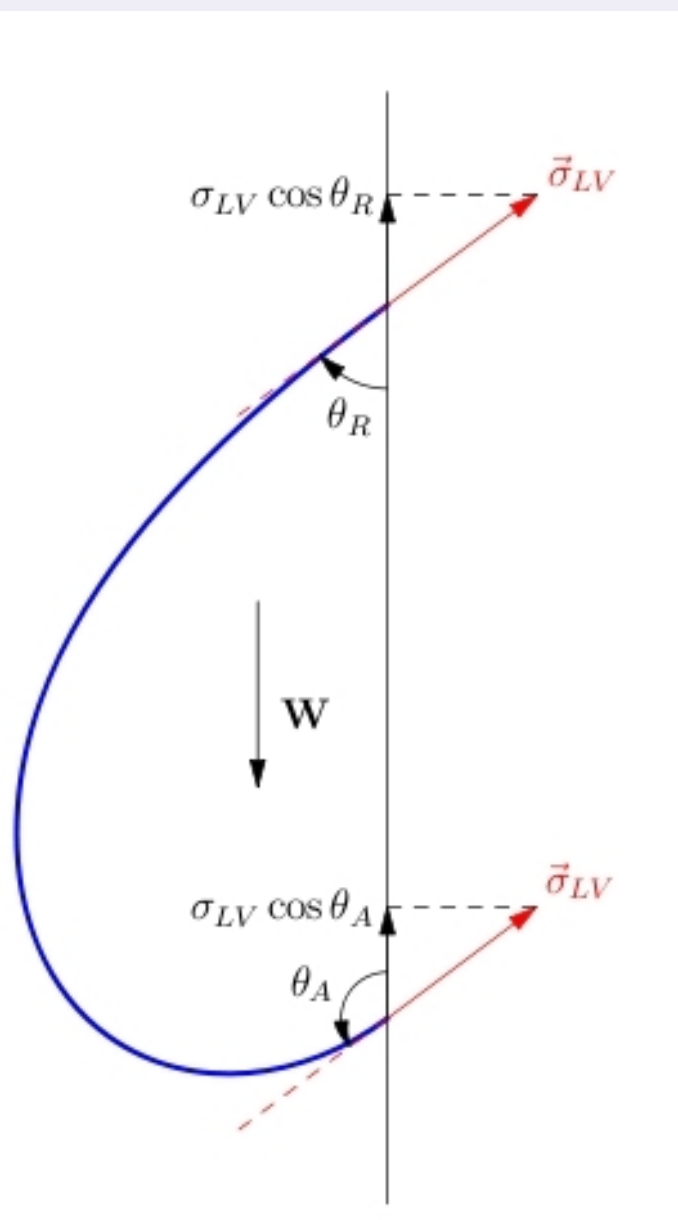
$$\rho g A + \sigma_{LV} \cos \theta_A - \sigma_{LV} \cos \theta_R \leq 0 \quad (1)$$

where  $\sigma_{LV}$  is the surface tension,  $\rho$  is the liquid density,  $\mathbf{g}$  is the usual gravity acceleration,  $A$  is the area of the drop and  $\theta_A$  and  $\theta_R$  are the *advancing contact angle* and the *receding contact angle*. The maximum value  $A_{crit}$  of  $A$  compatible with (1) is:

$$A_{crit} = \frac{\sigma_{LV}}{\rho g} (\cos \theta_R - \cos \theta_A) \quad (2)$$

Formula (2) prompts two remarks:

- necessary condition for adhesion is that  $\cos \theta_A \neq \cos \theta_R$  (i.e. Young's law is violated).
- $A_{crit}$  is proportional to  $(\cos \theta_R - \cos \theta_A)$ .



## 2. Mathematical approach

The energy of an homogeneous liquid drop  $\omega$  in contact with an homogeneous solid  $S$  and surrounded by a fluid is

$$E(\omega) = (\sigma_{SL} - \sigma_{SV})|\Sigma_{SL}| + \sigma_{LV}|\Sigma_{LV}| + \int_{\omega} G(\mathbf{x}) d\mathcal{V}_x + k$$

where  $|\Sigma_{SL}|$  is the measure of the solid-liquid interface,  $|\Sigma_{LV}|$  is the measure of the liquid-vapor interface,  $\sigma_{AB}$  is the surface tension on the  $AB$  interface,  $G(\mathbf{x})$  stands for a generic potential related to an external force field (gravity). Given a volume  $\mathcal{V} > 0$ , the geometric **capillarity problem** is to find the surface such that:

$$\omega^* = \underset{|\omega|=\mathcal{V}}{\operatorname{argmin}} \{E(\omega)\}.$$

## 3. The phase field approach

We are looking for  $\phi$  (the *phase function*), which equals one on the region occupied by the liquid. Given  $\Omega \subset \mathbb{R}^3$ , whose boundary  $\partial_S \Omega$  is the solid  $S$ , a potential  $W(\mathbf{s}) = a^2 s^2 (1 - s)^2$  (with  $a > 0$  to be specified later) and a continuous function  $\sigma : [0, +\infty) \rightarrow \mathbb{R}$  we define

$$E_\epsilon(\phi) = \int_{\Omega} \left( \epsilon |\nabla \phi|^2 + \frac{1}{\epsilon} W(\phi) + \phi G(\mathbf{x}) \right) d\mathbf{x} + \int_{\partial\Omega} \sigma(\tilde{\phi}) d\mathcal{H}_{n-1}(\mathbf{x})$$

We can extend  $E_\epsilon$  in  $L^1$  in the following way:

$$E_\epsilon(\phi) = \begin{cases} E_\epsilon(\phi) & \text{if } \phi \in H^1(\Omega, \mathbb{R}) \\ +\infty & \text{otherwise in } L^1 \end{cases} \quad (3)$$

Now, following Modica [2], if we consider

$$\hat{\sigma}(t) = \inf_{s \geq 0} \left\{ \sigma(s) + 2 \left| \int_t^s \sqrt{W(y)} dy \right| \right\}, \quad c_0 = \int_0^1 \sqrt{W(y)} dy$$

then  $E_\epsilon$   $\Gamma$ -converges to

$$\tilde{E}_0(\phi) = \begin{cases} 2c_0|\Sigma_{LV}| + \hat{\sigma}(1)|\Sigma_{SL}| + \hat{\sigma}(0)|\Sigma_{SV}| + \int_{\Omega} \phi(\mathbf{x}) G(\mathbf{x}) d\mathbf{x} & \text{if } \phi \in BV(\Omega, \{0, 1\}) \\ +\infty & \text{otherwise in } L^1 \end{cases}$$

and if  $\phi_\epsilon^*$  is a family of minimizers of  $E_\epsilon$ , and if  $\phi^*$  is its limit in  $L^1$ , then  $\phi^*$  is a minimizer for  $\tilde{E}_0$ .

If we choose  $\sigma(\mathbf{x}) := N\mathbf{x}$  (with this choice  $-2\epsilon \frac{\partial \phi}{\partial n} = N$  on  $\partial_S \Omega$ ) and set:

$$2c_0 = \frac{a}{3} = \sigma_{LV}, \quad \hat{\sigma}(0) = 0,$$

$$\hat{\sigma}(1) = \inf_{s \geq 0} \left\{ Ns + 2a \left( \frac{s^3}{3} - \frac{s^2}{2} + \frac{1}{6} \right) \right\} = \sigma_{SL} - \sigma_{SV}.$$

we can conclude that  $E_\epsilon$   $\Gamma$ -converges to the capillarity energy.

## 4. The solution scheme

The Euler-Lagrange equation for the phase field model is (for sake of simplicity we set  $\mathbf{G} = \mathbf{0}$  and  $a = 1$ ):

$$\begin{cases} -\epsilon \Delta \phi + \frac{1}{\epsilon} \phi(1 - \phi)(1 - 2\phi) + \lambda = 0 & \text{in } \Omega \\ \frac{\partial \phi}{\partial n} = -\frac{N}{2\epsilon} & \text{on } \partial_S \Omega \end{cases} \quad (4)$$

where  $\lambda$  is a lagrangian multiplier for the constraint  $\int_{\Omega} \phi = \mathcal{V}(\mathbf{t} + \delta \mathbf{t})$ . We transform (4) into a parabolic PDE generated by a gradient flow:

$$\phi_\tau = \epsilon \Delta \phi - \frac{1}{\epsilon} \phi(1 - \phi)(1 - 2\phi) - \lambda. \quad (5)$$

The solution will be  $\lim_{\tau \rightarrow +\infty} \phi(\tau, \cdot)$ .

## 5. The quasi-static evolutionary model for hysteresis

The capillarity energy can't describe the hysteresis effect: a necessary condition for stationarity is that Young's law is valid. So it's necessary to introduce a dissipative term able to capture the frictional effects. For a quasi-static evolutionary drop a new functional can be written:

$$\omega^*(\mathbf{t} + \delta \mathbf{t}) = \underset{|\omega|=\mathcal{V}(\mathbf{t} + \delta \mathbf{t})}{\operatorname{argmin}} \{E(\omega, \mathbf{t} + \delta \mathbf{t}) + D(\omega, \omega^*(\mathbf{t}))\}$$

where  $\omega^*(\mathbf{t})$  is the configuration at time  $t$

$D(\omega_1, \omega_2) = \mu |\partial_S \omega_1 \triangle \partial_S \omega_2|$  is the **dissipation**

$(A \triangle B) = (A \setminus B) \cup (B \setminus A)$

$\mu > 0$  is a parameter giving the dissipated energy per unit area.

From a mathematical point of view this description is equivalent to consider a bi-component solid surface; so we are going to solve:

$$\begin{aligned} \phi_\epsilon^*(\mathbf{t} + \delta \mathbf{t}) &= \arg \min \left\{ E_\epsilon(\phi, \mathbf{t} + \delta \mathbf{t}), \text{ subject to } \int_{\Omega} \phi = \mathcal{V}(\mathbf{t} + \delta \mathbf{t}) \right\} \\ \phi_\epsilon^* &= \begin{cases} N_A & \text{on } \partial_S \Omega_A^\epsilon \\ N_R & \text{on } \partial_S \Omega_R^\epsilon \end{cases} \end{aligned}$$

where  $\partial_S \Omega_R^\epsilon$  and  $\partial_S \Omega_A^\epsilon$  are  $\epsilon$ -approximations of the wet and the dry part of the solid, and  $N_A$  ( $N_R$ ) are the Neumann boundary condition associated with the advancing (receding) angle.

## 6. Numerical results

We checked the validity of the proposed model by determining the critical volume (that is the maximum value over which a drop is no longer in equilibrium) of water drops placed on differently treated vertical glasses, comparing and checking them against experiments by Shanahan [3]. The graph below shows the good agreement.

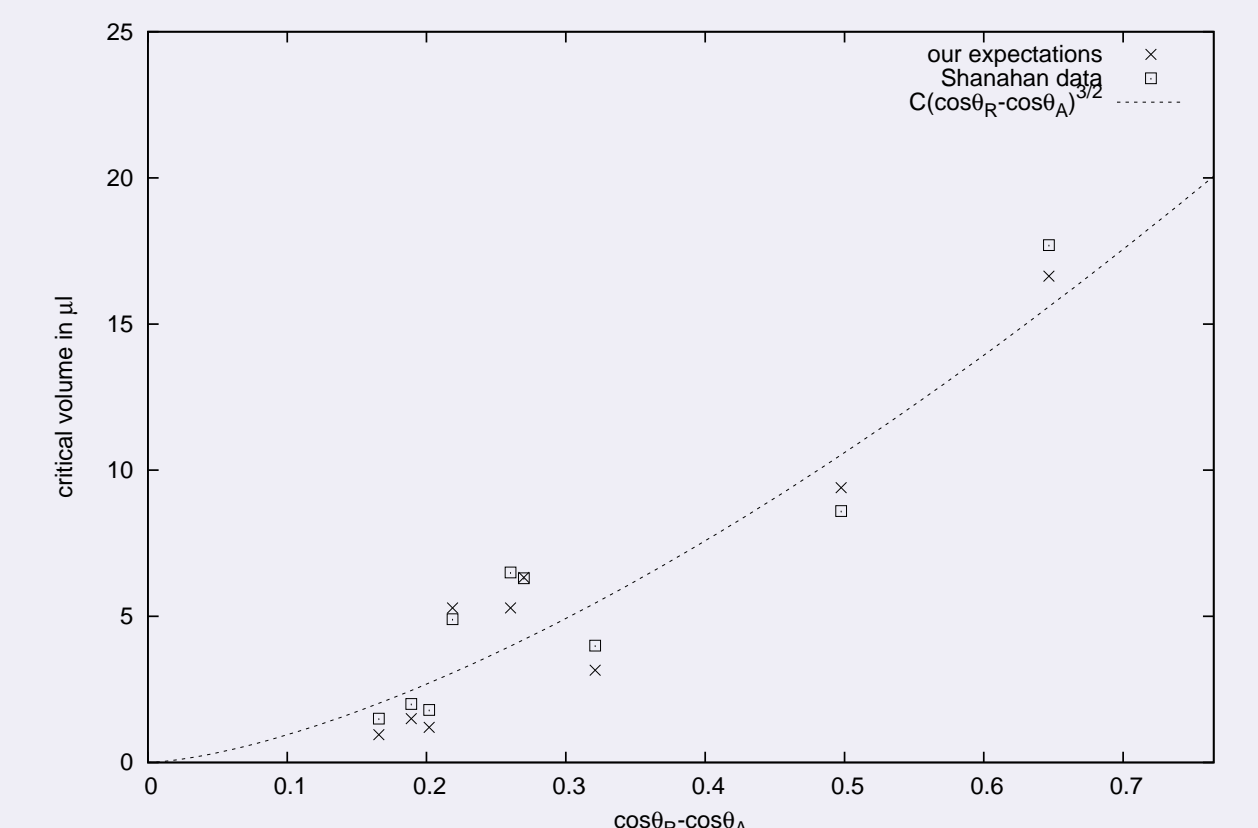
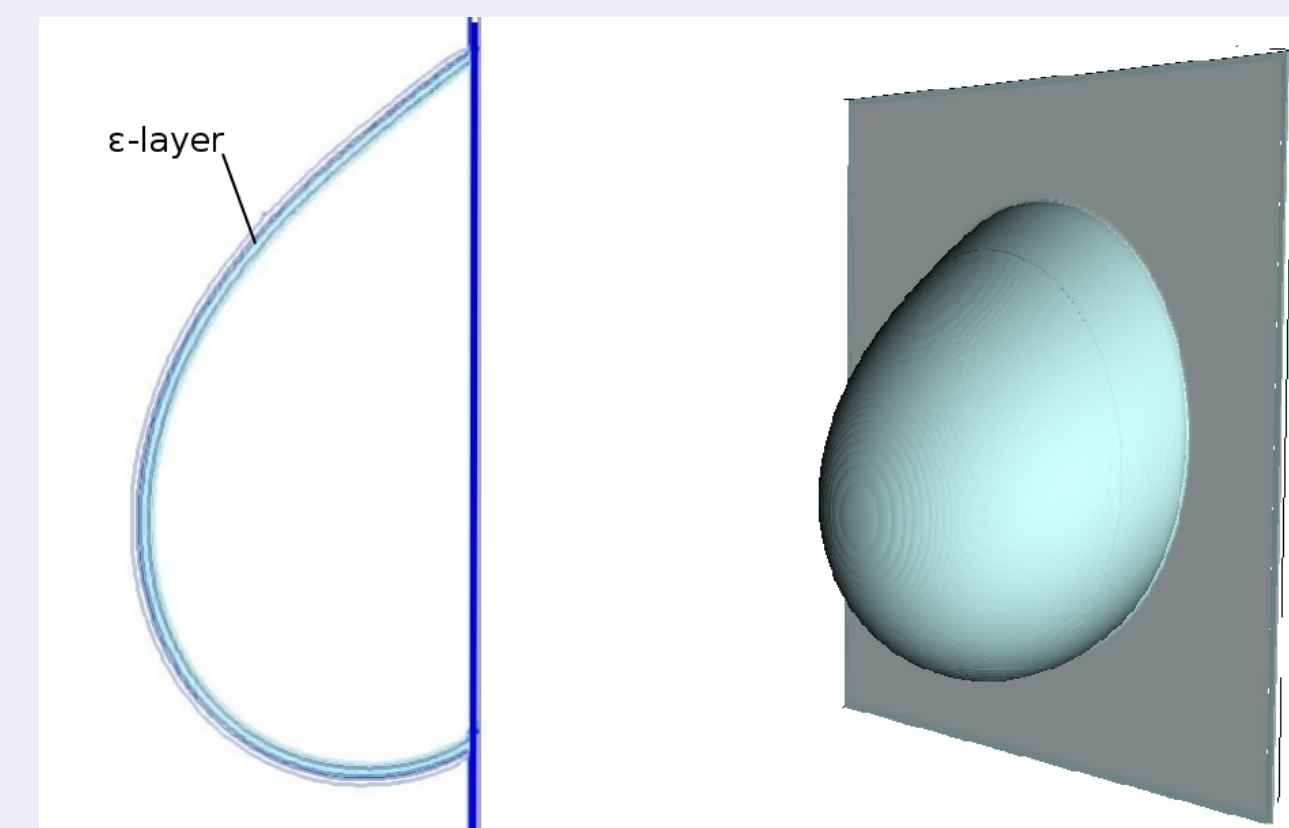


Figure: On the left a vertical slice and a 3-D picture of a phase field drop on a tilted plate; on the right the plot of the obtained results.

## References

1. A.DeSimone, L.Fedeli, A.Turco, *A phase field approach to wetting and contact angle hysteresis phenomena*, Proceedings book of IUTAM-Symposium on Variational Concepts with Applications to the Mechanics of Materials, Springer-Verlag, in press
  2. L. Modica, *Gradient Theory of phase transitions with boundary contact energy*. Ann. Inst. H. Poincaré Anal. Non Linéaire 5, 497 (1987)
  3. A. Carre and M.E.R. Shanahan, *Drop motion on an Inclined Plane and Evaluation of Hydrophobic Treatments to Glass*. J. Adhesion, 1995, Vol. 49, pp. 177-185
- The third image is taken from the review *Wetting and Roughness*, David Quéré, Laboratoire de Physique et Mécanique des Milieux Hétérogènes, ESPCI, 75005, Paris